

# CFD vs. lumped models applied to HAM: a comparison between HAM-Tools and Comsol

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## Abstract

CFD models have several advantages in comparison with zonal-models, due to the more accurate calculation of the airflow distribution within the built environment. Nevertheless, in currently available CFD software the simulation of mass transfer cannot be directly extended from the fluid region to the solid region. In the whole-building moisture transport studies, the mass coupling between the indoor environment and the wall system is usually achieved by third party programming. The Annex 41 research project of the International Energy Agency (IEA) was carried out to explore the complex physics governing the whole building heat, air and moisture (HAM) transfer, by developing several models to couple 3-D CFD simulations with hygrothermal models of walls.

The objective of this study is to develop a coupled CFD model able to simulate the HAM transport in a single environment (i.e. a simple test room), influenced by the room factors. A numerical method was utilized to model the indoor environment and the moisture transport process in the simple room and inside the wall system as influenced by the moisture loads and ventilation conditions.

The comparison between the CFD and a lumped model allows us to demonstrate how a simplified model can be reliable in predicting the RH variation inside a room, also taking into account the indoor material buffering effect.

## 1. Introduction

HAM-Tools is a building simulation software implemented on the Simulink-Matlab platform by the Chalmers University of Technology (Gotheborg, Sweden) and the Technical University of Denmark (Lygby, Denmark) within the Annex 41 project. The main objective of this tool is to run simulations of transfer processes related to building physics, i.e. heat and mass transport in buildings and building components in operating conditions. Nevertheless, results from literature demonstrate how simulations made with the HAM-Tools lumped model over-estimate about twice the moisture dampening effect than what was actually measured experimentally (Ramos et al., 2012). The authors then focused on the air-flow pattern, comparing experimental measurement results to theoretical ones. An appreciable difference between the measured hygroscopic inertia and the calculated one was found due to the air velocity field that caused the development of several dead zones inside the test chamber. This meant that the perfect mixing of the room air, a simplification commonly assumed in HAM simulations, had a clear impact on the results of this kind of problem. If perfect mixing is assumed, all the hygroscopic surfaces would be fully active; but since this is not true, the flux chamber simulations overestimated the moisture buffering effect.













## 6. Acknowledgement

This work was carried out within a research activity supported by Saint-Gobain PPC Italia S.p.A. about the *Influence of hygroscopic interior finishing on indoor comfort conditions*.

## 7. Nomenclature

### Symbols

$D_{\varphi}$	liquid conduction coefficient (kg/ms)
$c_p$	specific heat capacity (J/kgK)
$\dot{g}_a$	density of air flux (kg/m <sup>2</sup> s)
$\dot{g}_v$	density of moisture flux (kg/m <sup>2</sup> s)
$H$	volumetric heat capacity (J/m <sup>3</sup> K)
$h_v$	evaporation enthalpy of water (J/kg)
$T$	absolute temperature (K)
$t$	time (s)
$p_c$	suction pressure (Pa)
$p_v$	vapour pressure (Pa)
$p_{v,s}$	vapour pressure at saturation (Pa)
$u$	moisture content by mass (kg/kg)
$w$	moisture content by volume (kg/m <sup>3</sup> )
$x$	thickness (m)
$\delta_p$	vapour permeability (kg/m s Pa)
$\lambda$	thermal conductivity (W/m K)
$\lambda_l$	liquid conductivity (s)
$\rho_0$	density of dry material (kg/m <sup>3</sup> )
$\varphi$	relative humidity (-)
$\xi$	moisture storage capacity (kg/m <sup>3</sup> )

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