

3.2 Comfort variations in Pareto's solutions

The previous paragraphs show a good robustness of the MOO method to the epistemic uncertainty introduced by the choice of solar models. However, substantial differences can be highlighted when assessing the comfort performance. The thermal comfort indicators used for the investigation is the discomfort weighted time (WDT) index, as proposed by the EN 15251 (CEN, 2007c) through the degree hours criteria. The graph in Fig. 4 clearly shows the WDT variations of REF1 semi-detached house caused by the choice of the models when NPV and EP are chosen as objectives. This greater sensitivity of WDT to solar models has repercussions on the robustness of MOO procedure when three different goals such as NPV, EP and WDT are considered. The Pareto's fronts in Fig. 5 show a greater dispersion of the results obtained with the three different combinations of solar models. In this case, therefore, the choice of a combination of models leads to the selection of different optimal mix of ESMs.

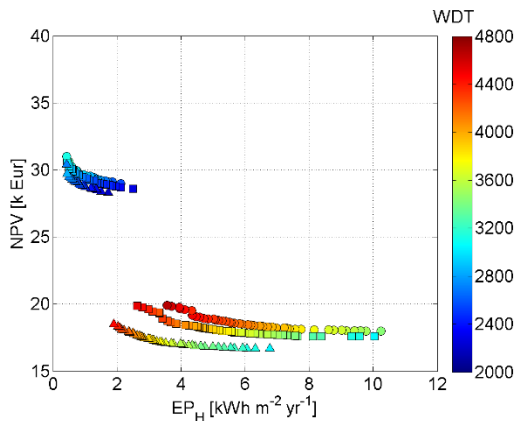


Fig. 4 – Pareto's fronts of the semi-detached house REF 1 with south oriented windows. The data points are colored according to WDT while circle referred to C1, square to C2 and triangle to C3.

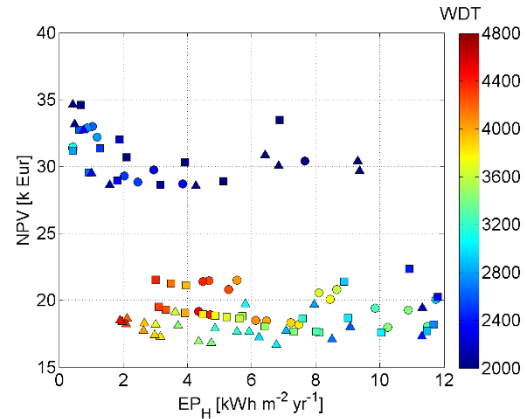


Fig. 5 – Pareto's fronts of the semi-detached house REF 1 with south oriented windows obtained with a 3 objective optimization. The data points are colored according to WDT while circle referred to C1, square to C2 and triangle to C3.

4. Conclusion

This work assessed the robustness of NSGA II in finding optimal building energy refurbishment when three different couples of solar irradiation models are adopted. The results show the variability of the EP index in the range of $\pm 3\%$ for most of the test cases for the simulation performed on the initial state.

As regards Pareto's fronts, the utilization of the C1 models makes some solutions not-dominated instead of dominated as they are for in cases C2 and C3. In particular, these new optimal solutions have higher insulation thickness and triple glazings due to the lower incident solar irradiation provided by C1 models.

Notice that slight differences are present in the mix of ESMs able to guarantee either the minimum NPV or the minimum EP. Again, the greatest differences occur with C1, which tends to increase the thickness of the insulating layers for both the optima.

The NSGA-II then shows a good robustness when the solutions are optimized in terms of NPV and EP. In fact, substantial changes are noted on the thermal discomfort of optima solutions. This greater sensitivity of the WDT index to solar irradiation implies a decrease of MOO robustness when the minimization of WDT becomes an objective.

5. Nomenclature

Symbols

A	area (m ²)
COND	Condensing boiler
DH	Double glazing with high SHGC
S	Surface of dispersing envelope (m ²)
SG	Single Glazing
SHGC	Solar heat gain coefficient (-)
STD	Standard boiler
TH	Triple glazing with high SHGC
V	Conditioned volume (m ³)

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